

In Span Hinge Replacement and Seismic Retrofit of the Flamingo Viaduct

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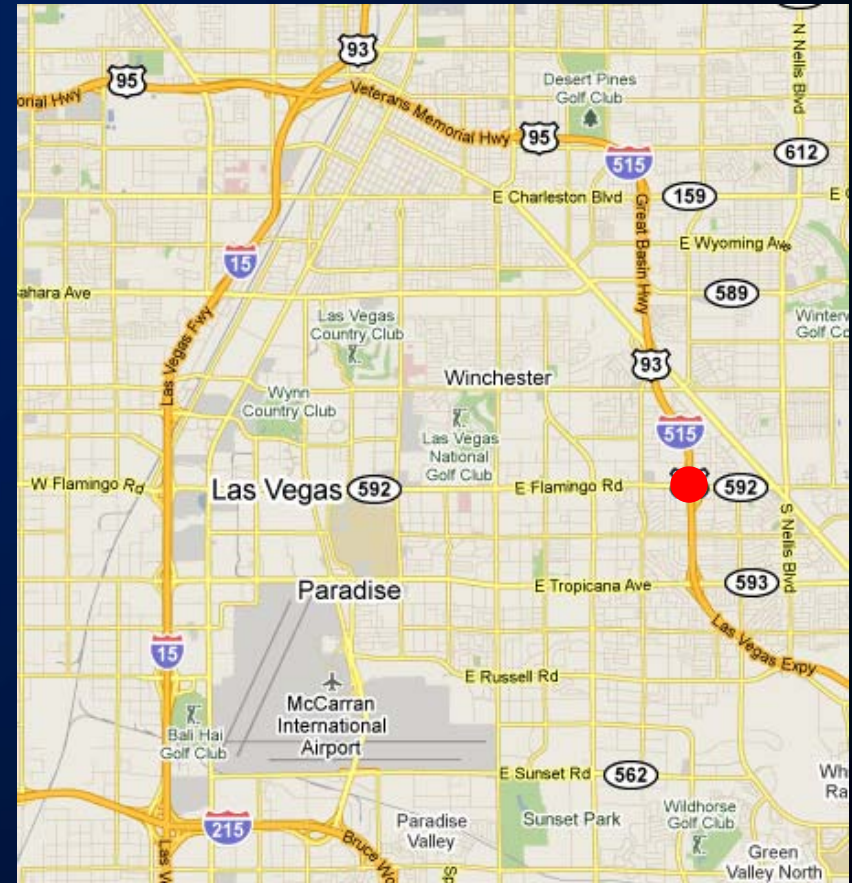
Sami Megally, Ph.D., PE

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Presentation Outline

- ▣ Nevada Background
- ▣ Flamingo Viaduct
 - Project History
 - Structural Assessment
 - Seismic Strategy
 - Design Challenges
 - Construction



Nevada Seismicity??

	Mag >= 7.0	Mag >= 6.0	Mag >= 5.0	Mag >= 3.5
1st	Alaska	Alaska	Alaska	Alaska
	59	370	2050	14914
2nd	California	California	California	California
	16	114	675	10965
3rd	Nevada	Hawaii	Nevada	Hawaii
	4	29	159	2247
4th	Hawaii	Nevada	Hawaii	Nevada
	4	21	80	1586
5th	Missouri	Montana	Washington	Washington
	2	6	41	898
6th	Arkansas	Washington	Montana	Idaho
	2	5	25	613
7th	Washington	Wyoming	Wyoming	Wyoming
	1	5	22	392
8th	Montana	Idaho	Idaho	Montana
	1	4	18	321
9th	South Carolina	Oregon	Utah	Utah
	1	3	15	193
10th		Arkansas	Oregon	Oregon
		3	14	148



USGS

UNR Seismology



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Retrofit

- ▣ **State adopted seismic prioritization**
 - Importance and vulnerability
 - Life Safety or better

- ▣ **1971 San Fernando→**
 - 1986 Caltrans Phase 1 (completed in 2000)
- ▣ **1989 Loma Prieta→**
 - Caltrans increased research
 - NDOT begins prioritization in early 1990's
- ▣ **1994 Northridge**
 - Caltrans Phase 2, Caltrans toll, CA Local

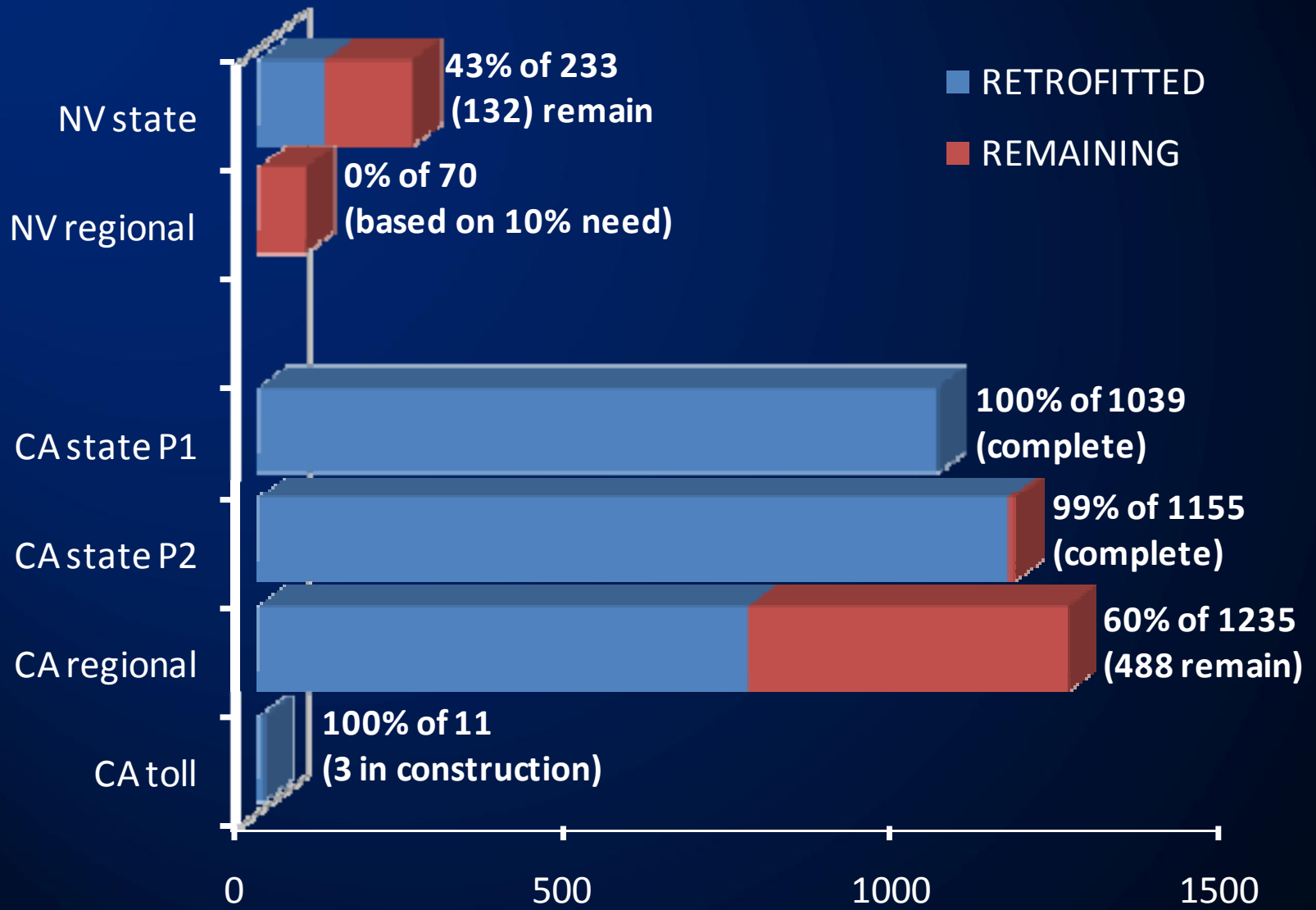
In-Span Hinge Failures

1971 San Fernando



1994 Northridge



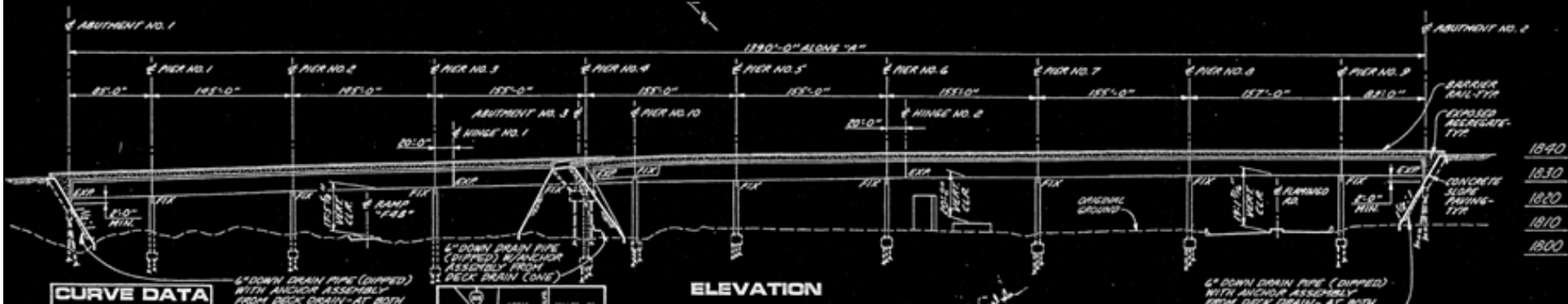
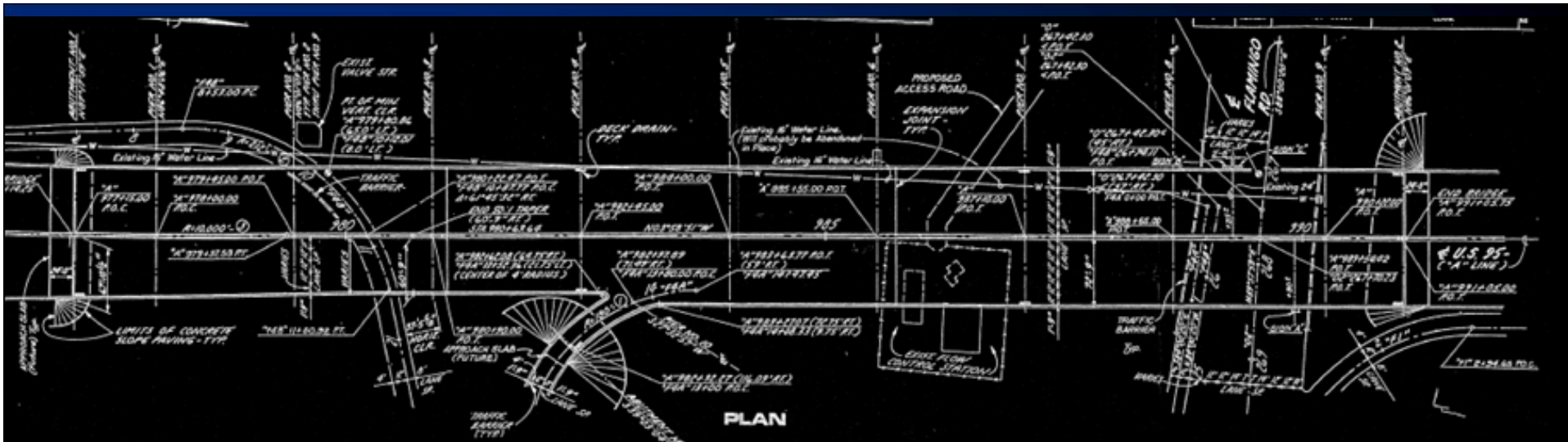


Bridges identified with seismic retrofit need



Flamingo Viaduct

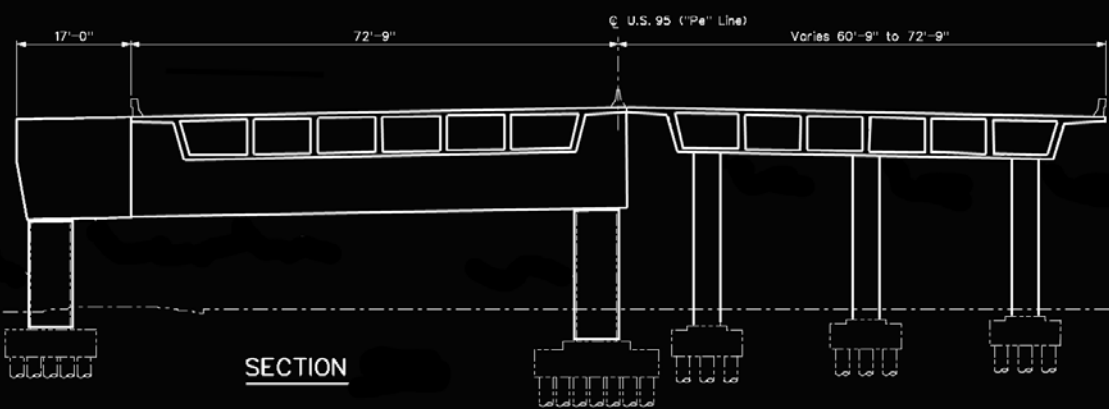
- ▣ Las Vegas, NV, I-515 over Flamingo
- ▣ Owner: Nevada DOT
- ▣ Constructed in 1982
- ▣ 10-span continuous PT box girder
- ▣ Twin 72ft wide 1400ft structures with 2 ISH
- ▣ Scope: Repair hinges, seismic retrofit/rehab
- ▣ \$3.5M Retrofit/Rehab (small cost difficult task)



CURVE DATA

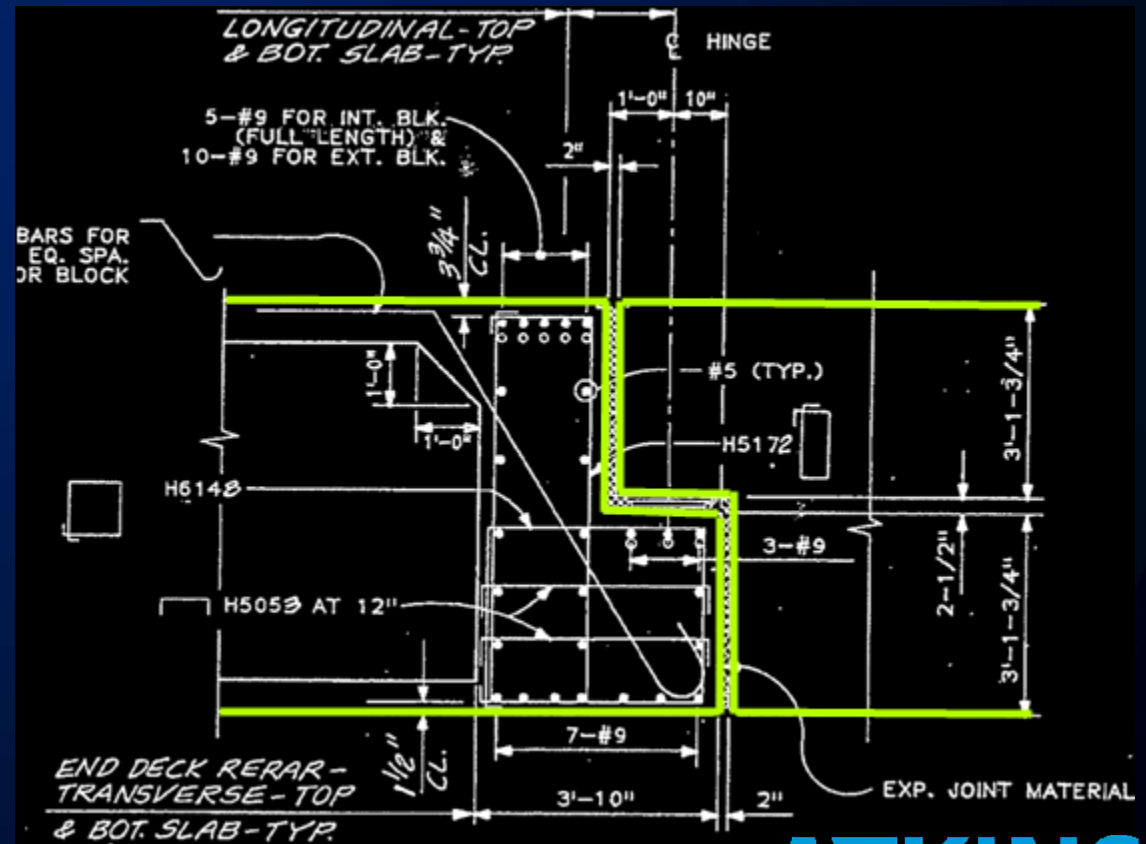
5" DOWN DRAIN PIPE (DIMMED) WITH ANCHOR ASSEMBLY FROM DECK DRAIN-AT BOTH

5" DOWN DRAIN PIPE (DIMMED) WITH ANCHOR ASSEMBLY FROM DECK DRAIN (ONE)



Observed Issues

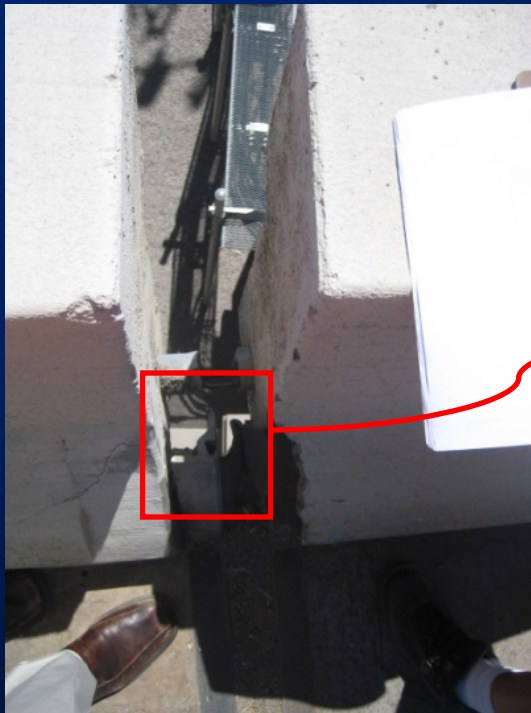
- Excessive hinge movement (18" seat)
 - Designed for 2in, measured 8-10 in
 - Restrainers failed
 - Hinge seats
 - Columns hinged
 - Cap beam T & V



In-Span Hinge



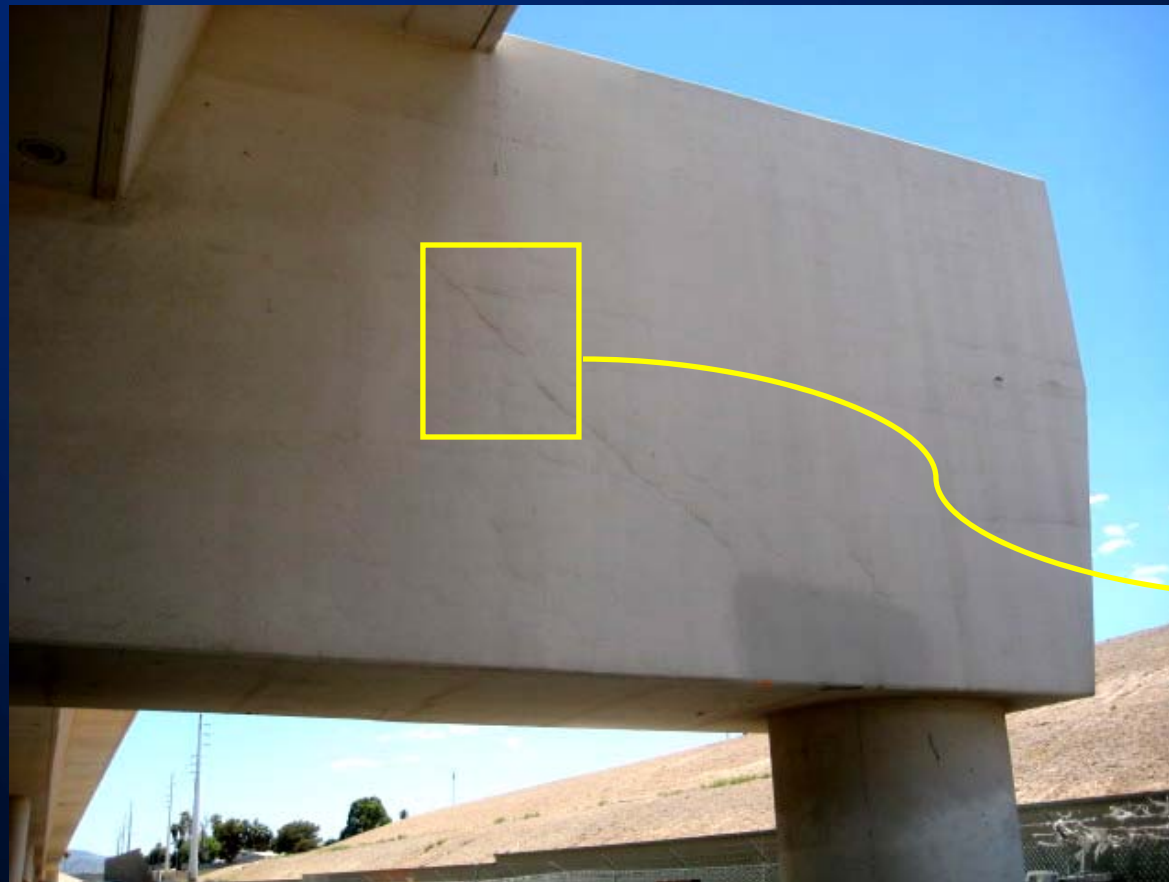
Bridge Rail Separation



Column Plastic Hinging



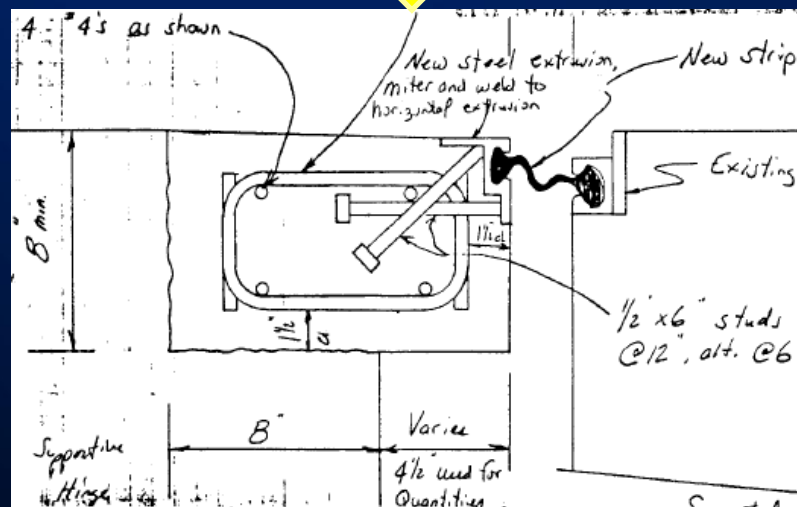
Outrigger T/V Cracking



Timeline

- ▣ 1985 inspection reports noted excessive ISH movement
- ▣ 1992 expansion joints reconstructed
- ▣ 2003 Initial rehabilitation study (PB)
- ▣ 2007 Second Rehabilitation study (PBSJ)
- ▣ 2010 Retrofit/Rehabilitation Type Selection and Final Design
- ▣ (9 year project)

1992 Expansion Joint Reconstruction



2007 Study

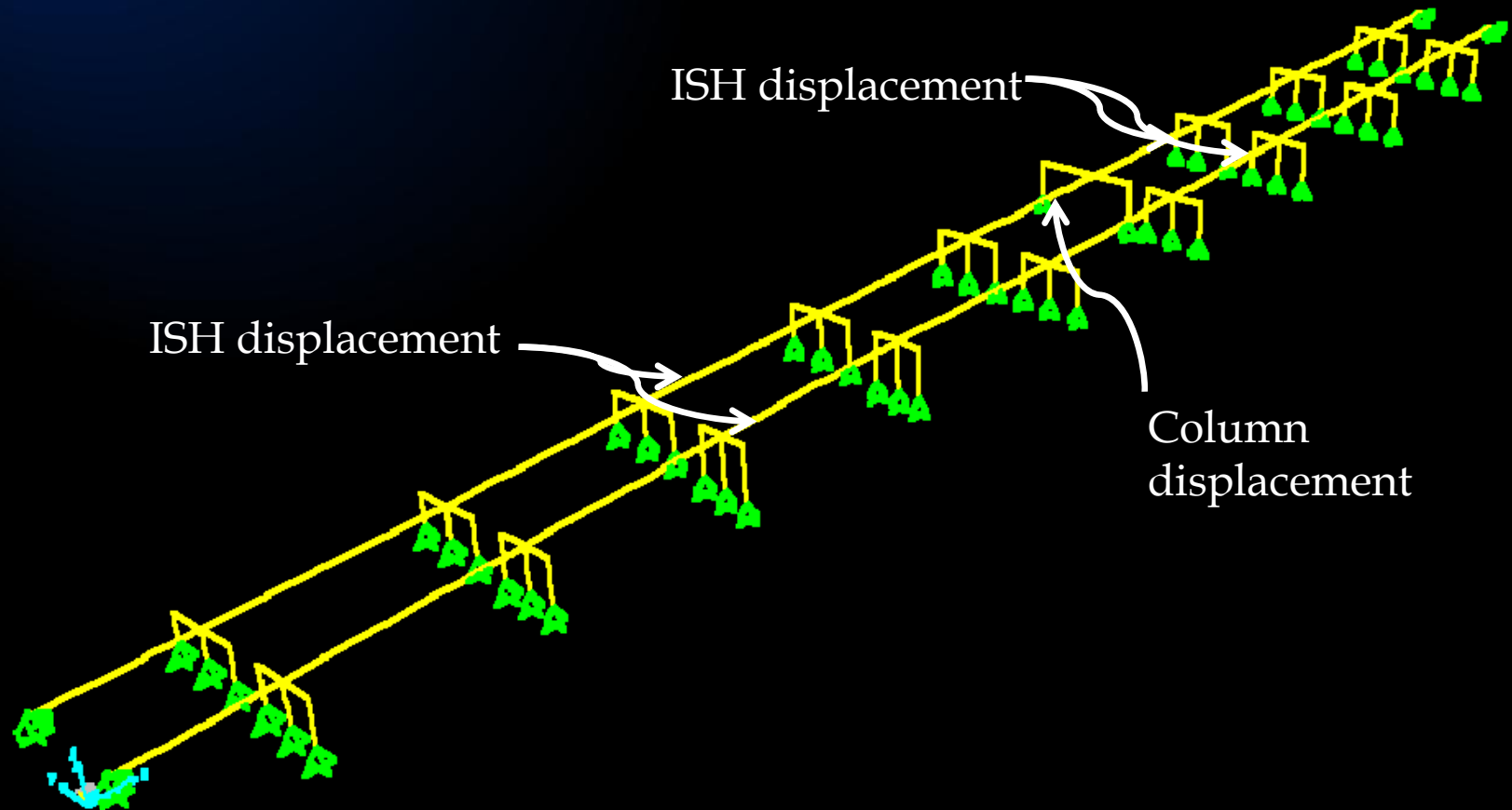
Location	Case 1 Calculated Opening (in)	Case 2 Calculated Opening (in)	Case 3 Calculated Opening (in)	Average Field Measured Opening (in)
NB Hinge 1	7.63	8.08	8.32	8.19
NB Hinge 2	7.17	7.58	7.8	8.44
SB Hinge 1	7.86	8.33	8.59	8.19
SB Hinge 2	6.99	7.38	7.58	8.13
Case 1 - 3in initial + long term placed 12 weeks after stressing + thermal				
Case 2 - 3in initial + long term placed 6 weeks after stressing + thermal				
Case 3 - 3in initial + long term placed 4 weeks after stressing + thermal				

- ▣ Original design did not account for creep/shrinkage
- ▣ Seismic = 7.5in, remaining effective seat = 8-10 in
- ▣ 30 columns were pushed beyond Δ_y
- ▣ Outrigger bent has torsional/shear D/C issues
- ▣ Three concepts were developed

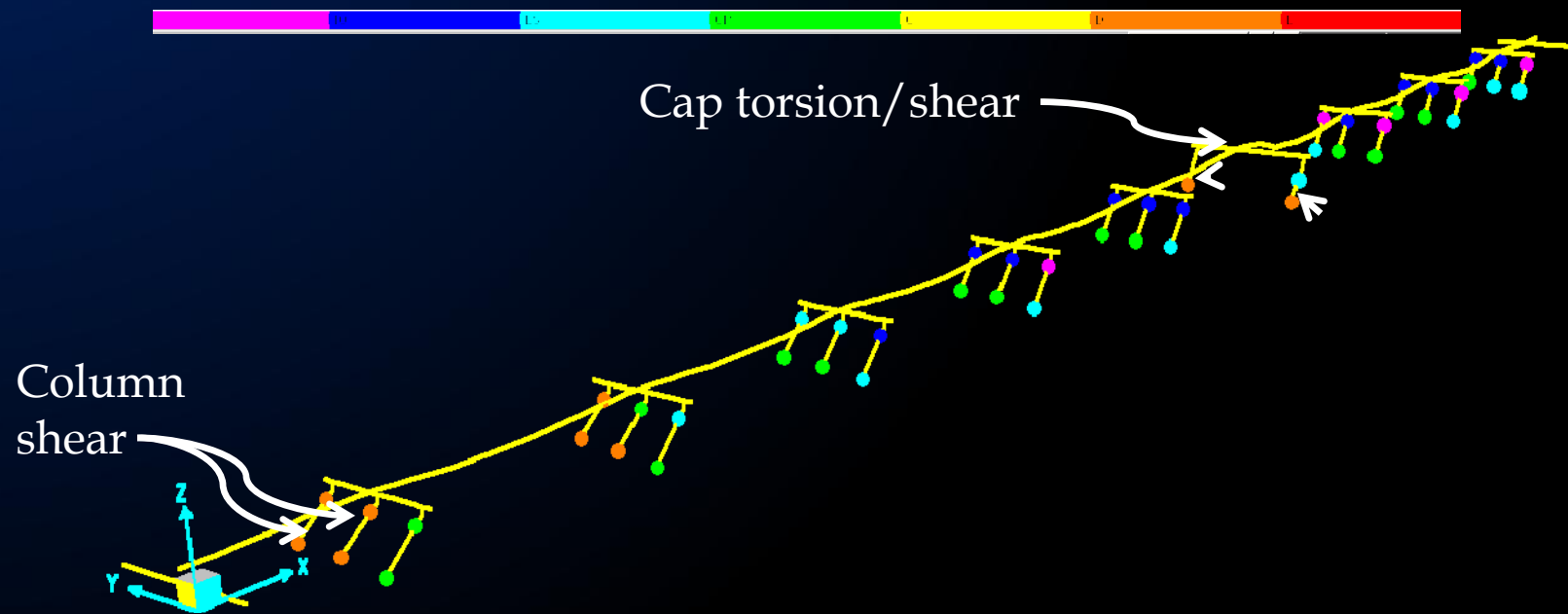
Seismic Analysis to Finalize Strategy

- ▣ Criteria is Life Safety
- ▣ Columns already experienced displacement
- ▣ NDOT standard is FHWA manual
 - Method B, C, D
- ▣ Caltrans standard (FHWA D) makes sense
 - “Linear” RSA displacement demands (ATC6)
 - NL pushover disp. capacities & force demands
- ▣ Add shortening deformations to 100/30 seismic demand, $\Delta_c > \Delta_d$

Linear RSA System



Nonlinear System Pushover



Hinge Rehab Options

- ▣ Existing bearings failed
- ▣ Insufficient seat width

- ▣ 3 Options investigated
 - Internal Strong Back (similar to CT seat extender)
 - External Strong Back
 - Complete Reconstruction
- ▣ Appearance, MOT, invasiveness, reliability

Major Factors to Consider

Environmental

Funding

Safety

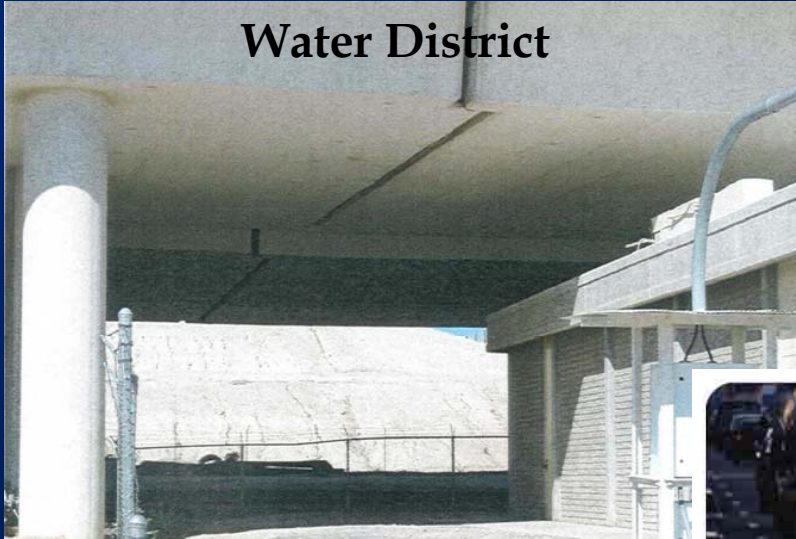
Politics

Right-of-way

Function

Project Constraints

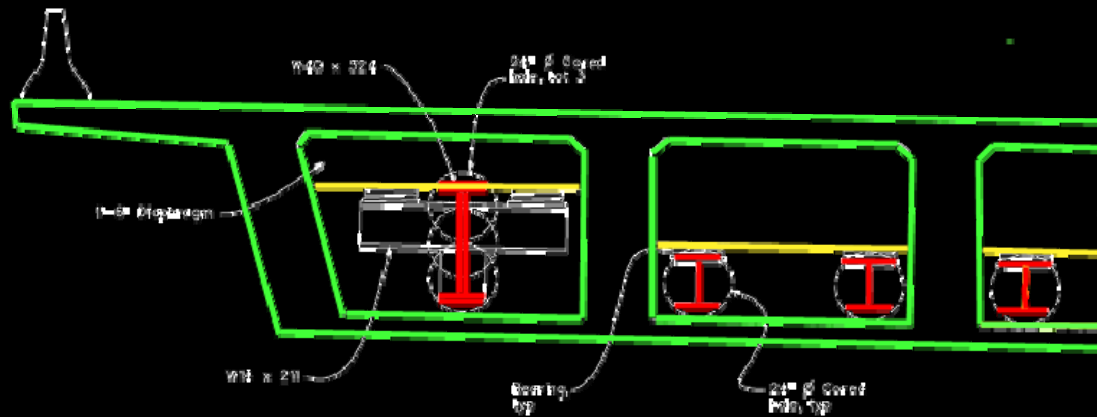
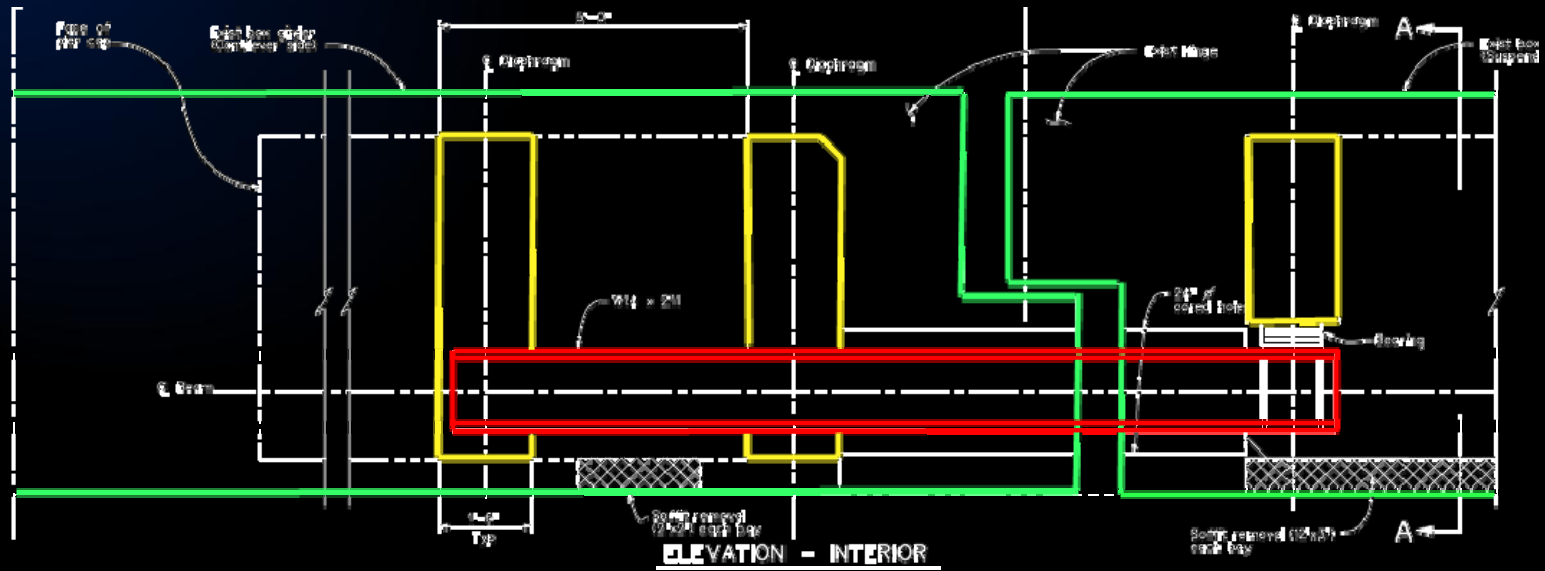
Water District



Traffic



Internal Strong Back



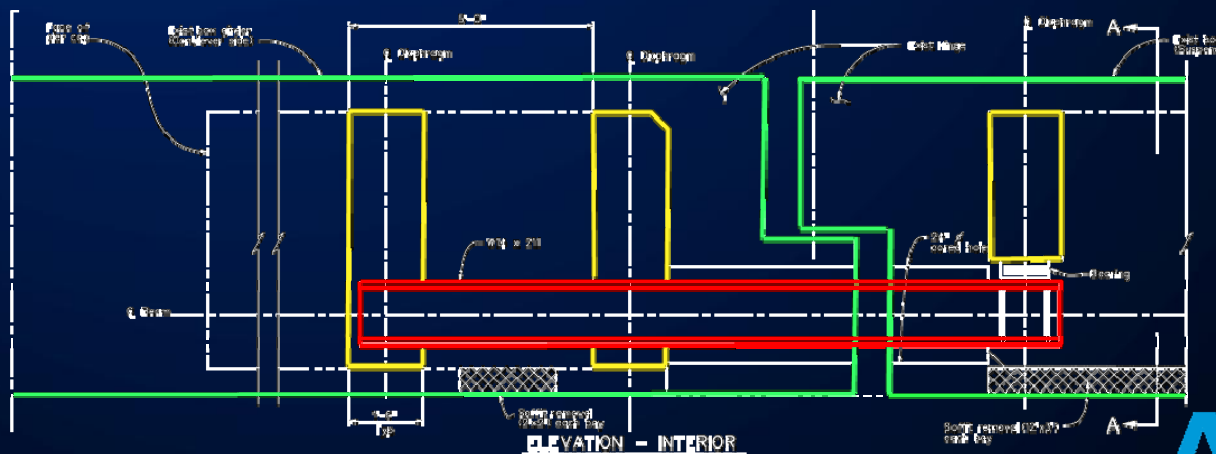
SECTION A-A

ADVANTAGES

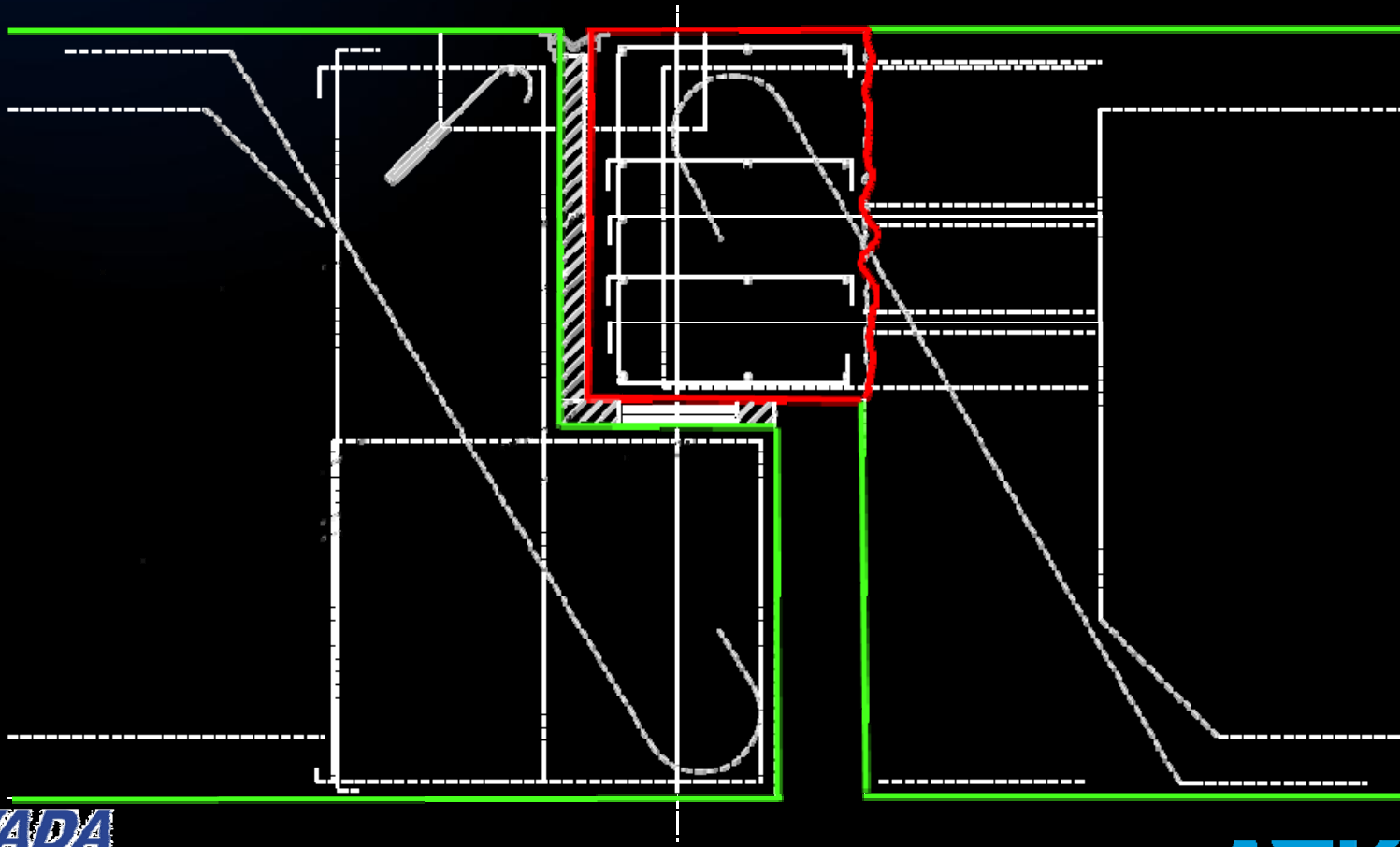
- ✓ Minor Traffic Impact
- ✓ No Future Maintenance
- ✓ No Impact on Bridge Aesthetics
- ✓ Bearing Pads Accessible for Inspection

DISADVANTAGES

- × Complex Structural Modification



Hinge Replacement

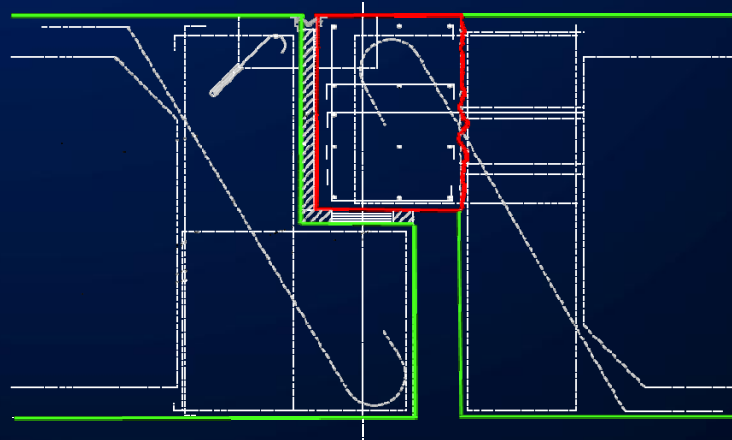


ADVANTAGES

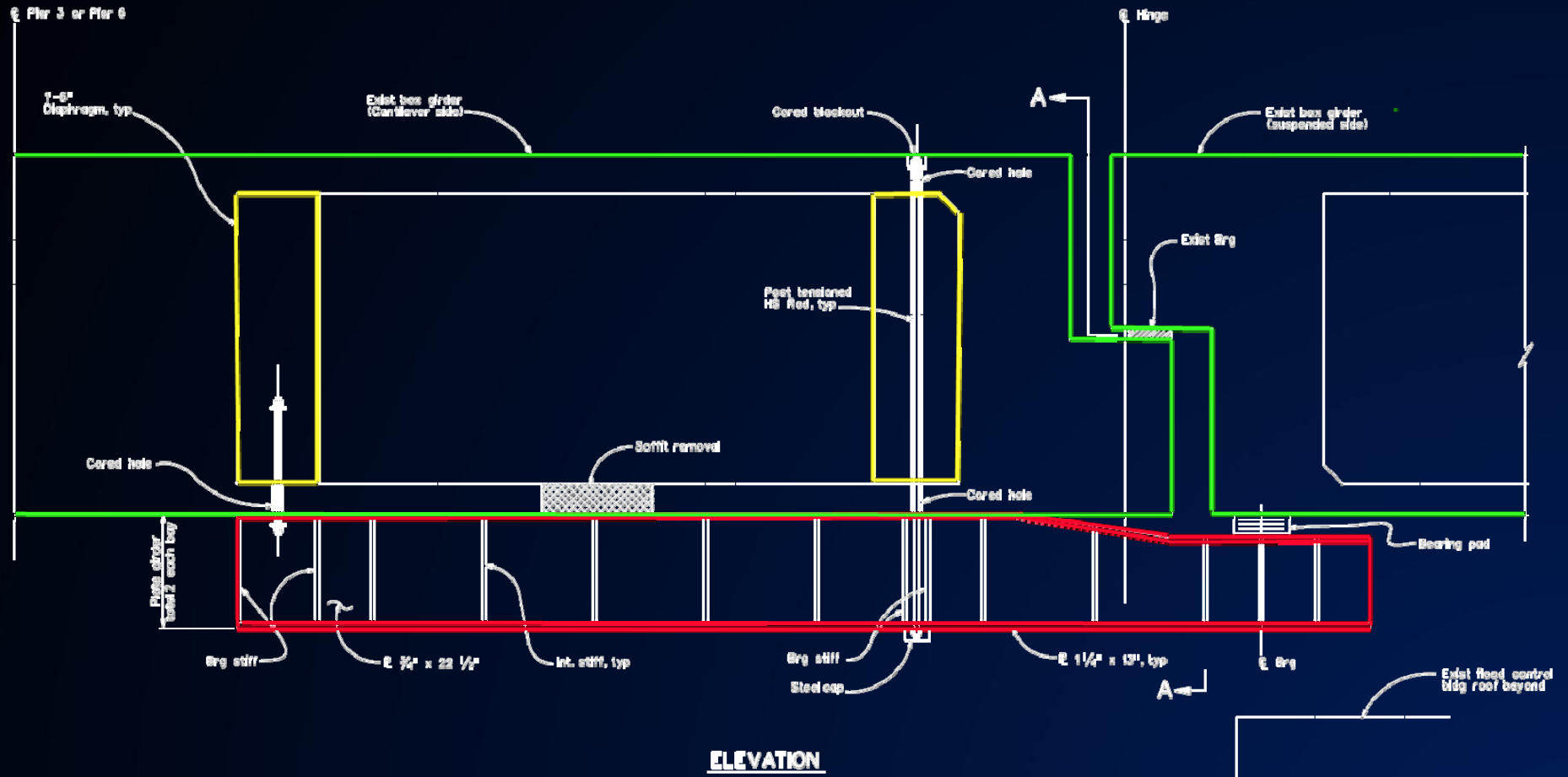
- ✓ No Future Maintenance
- ✓ No Aesthetic Impact

DISADVANTAGES

- × Complex Structural Modification
- × Significant Impact to Traffic
- × High Cost
- × Bearing Pads Inaccessible



External Strong Back

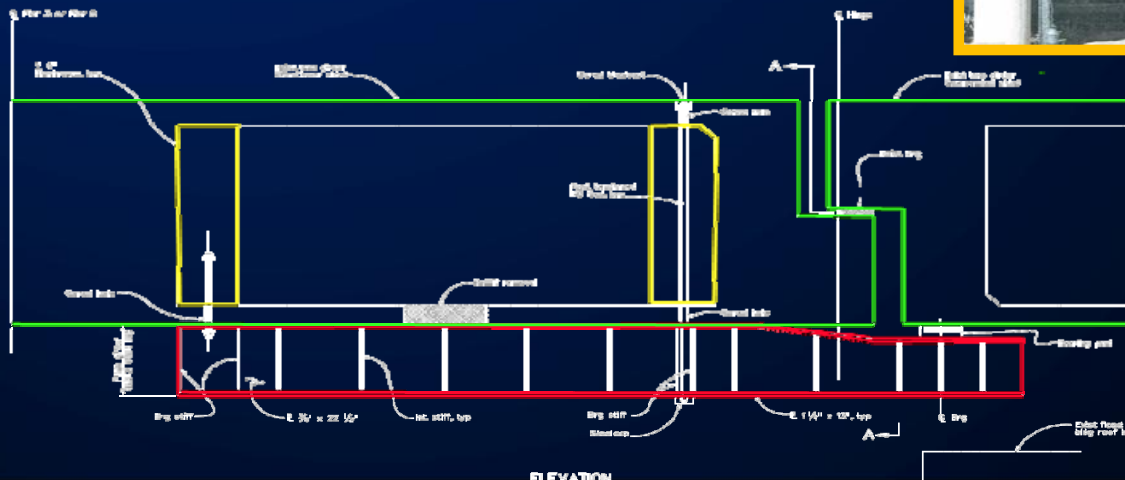


ADVANTAGES

- ✓ Ease of Construction
- ✓ Low Cost
- ✓ Minor Traffic Impact
- ✓ Bearing Pads Accessible for Inspection

DISADVANTAGES

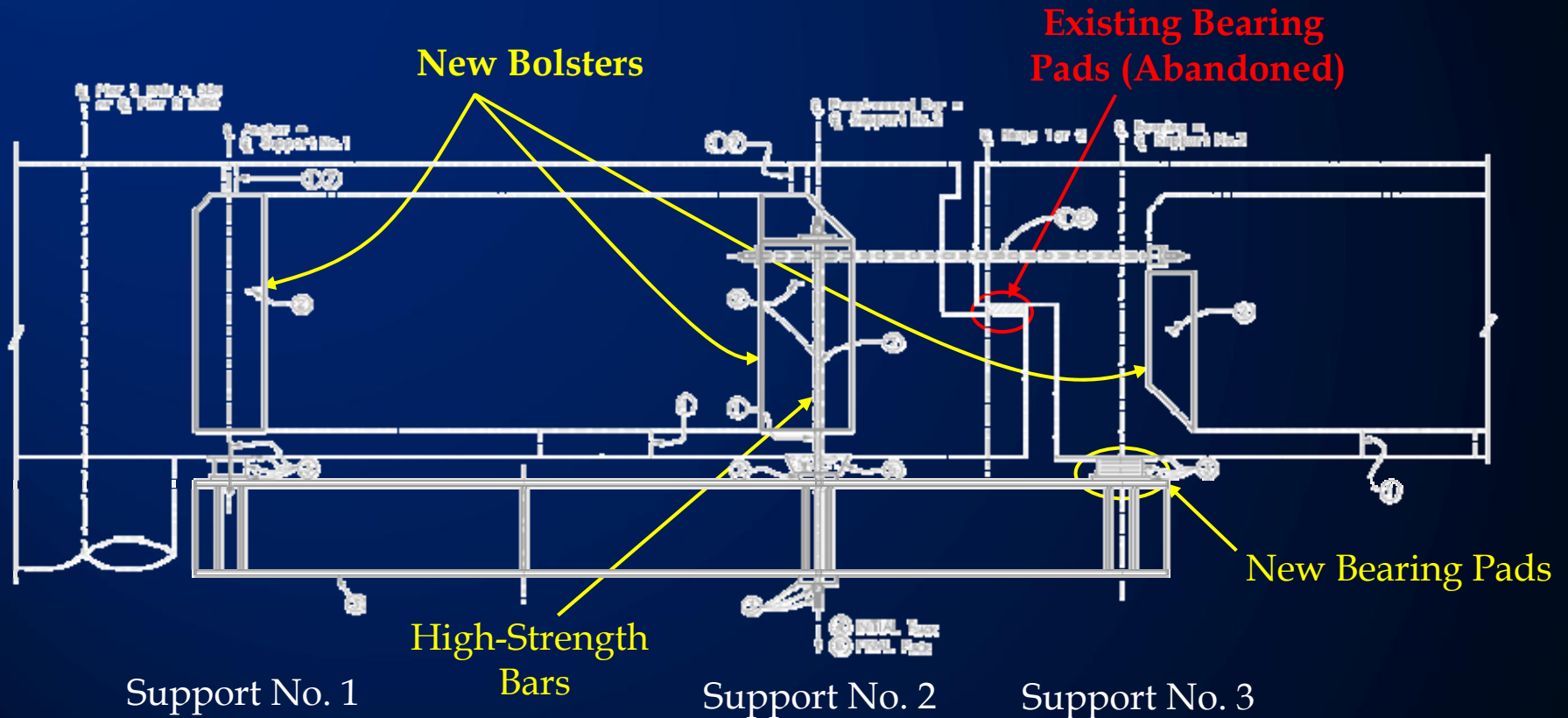
- × Aesthetics
- × Future Maintenance



Rehabilitation/Retrofit Design

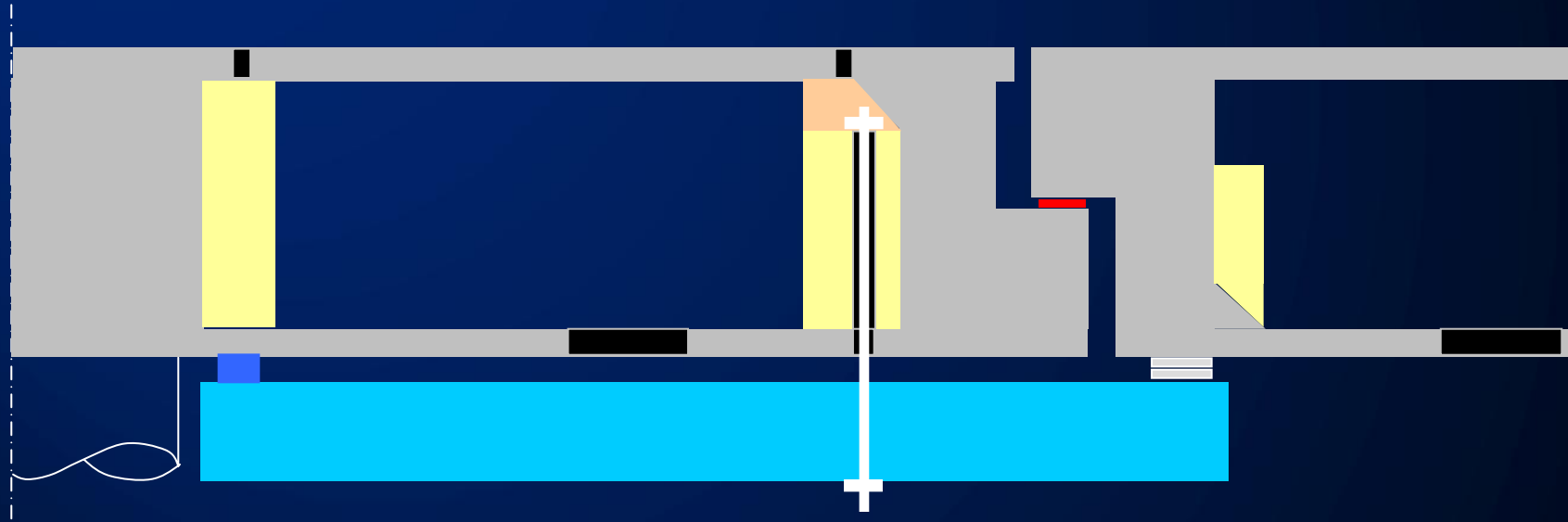
- Rehabilitation Overview
- Construction Sequence
- Rehabilitation Design Challenges
- Check of Existing Structure
- Seismic Assessment & Retrofit

Hinge Rehabilitation

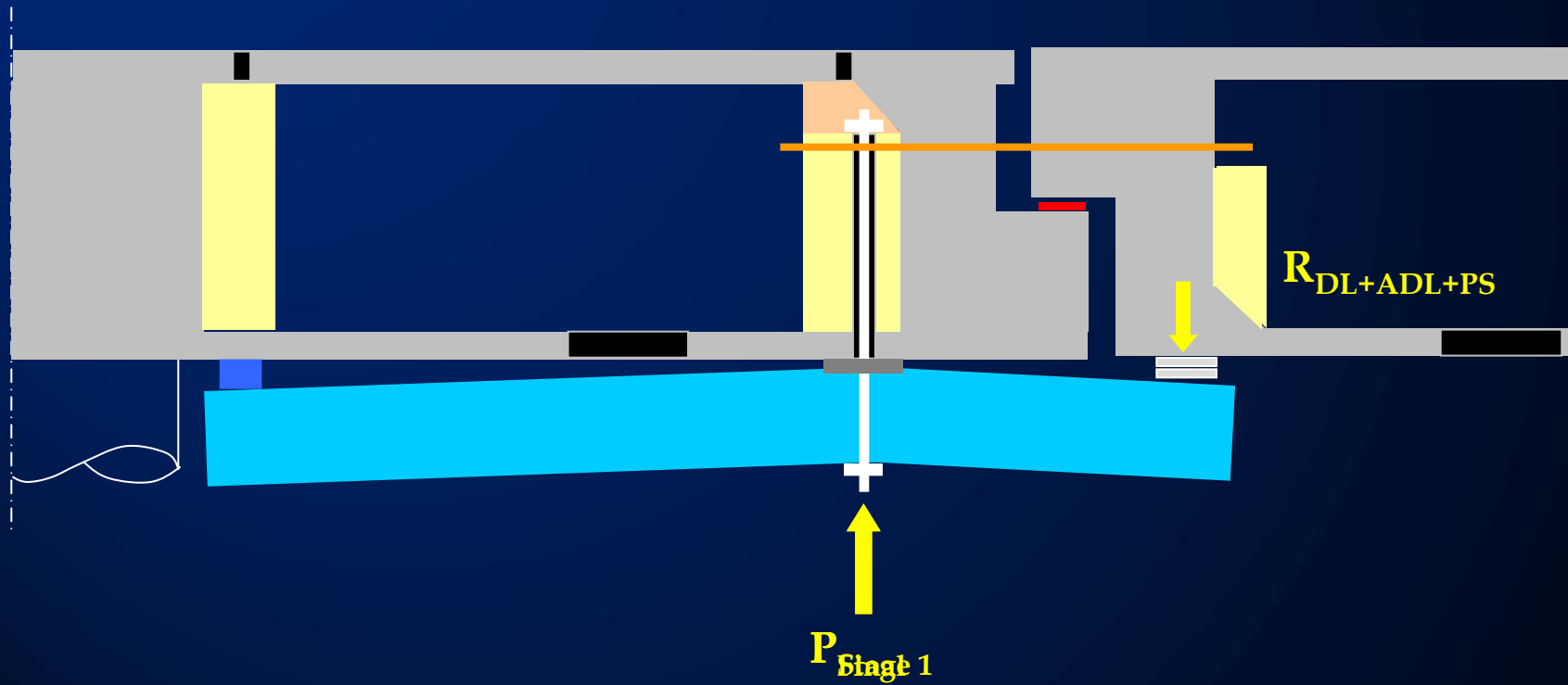


- New bearing pads are active for permanent loads reactions
- New bearing pads designed to take full live load reactions

Hinge Rehabilitation Construction Sequence



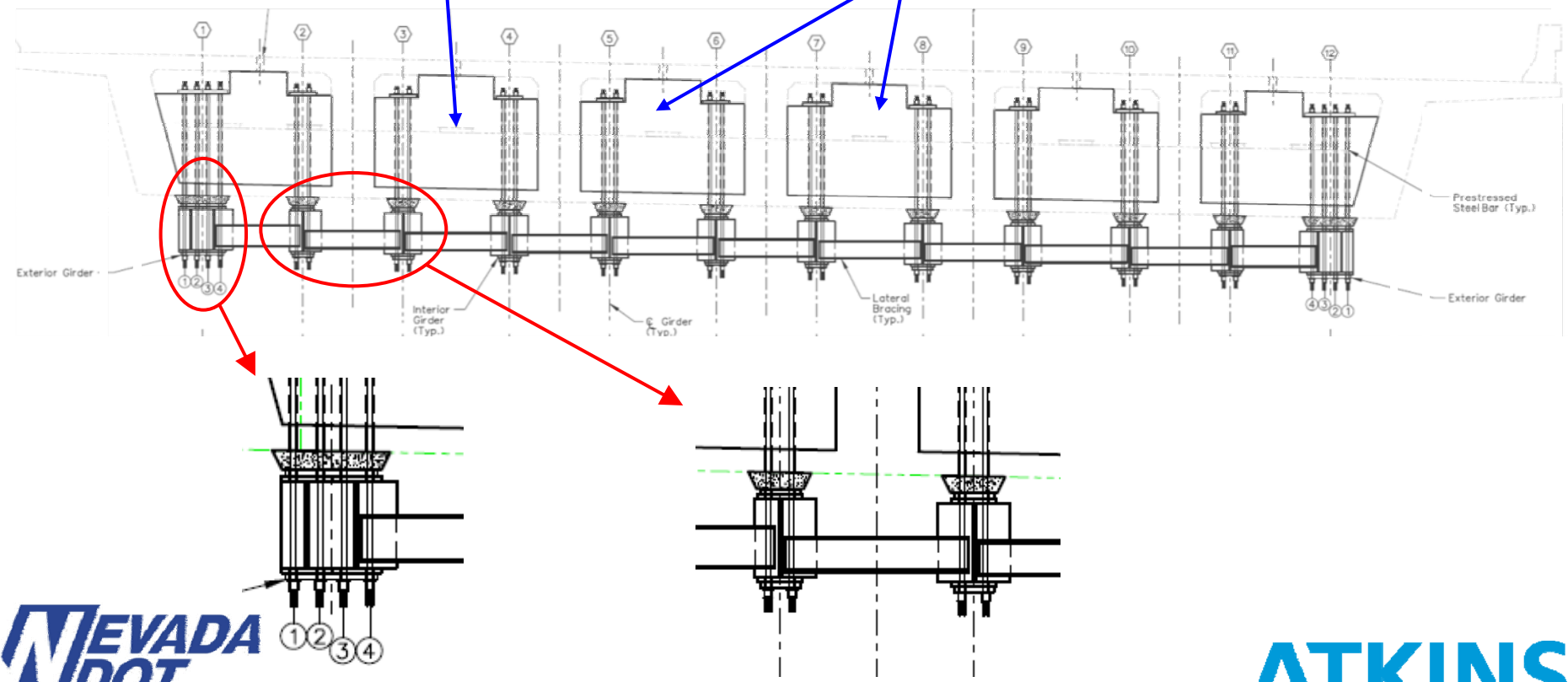
Hinge Rehabilitation Construction Sequence



PT Bars Stressing Sequence

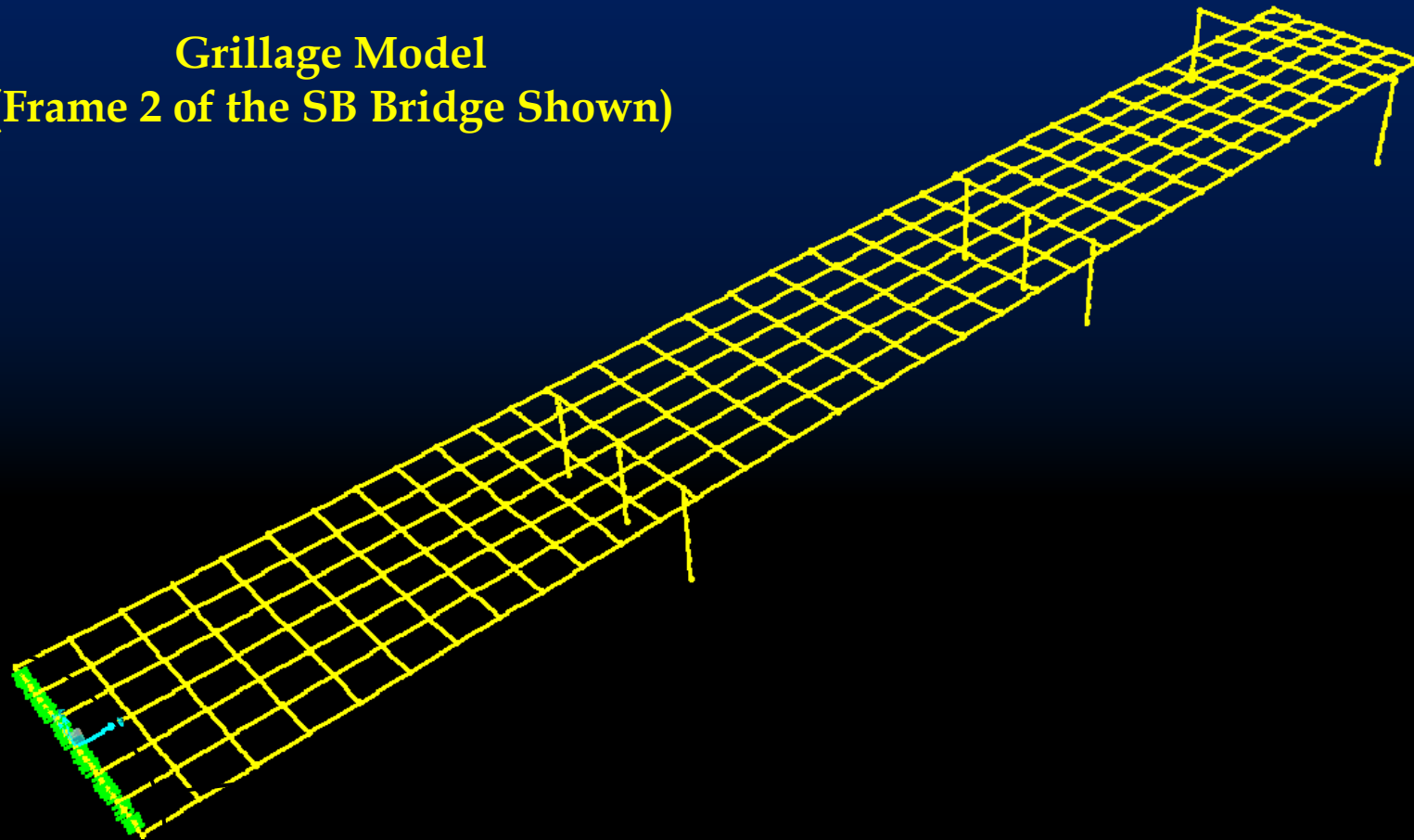
- PT bars are NOT stressed simultaneously at all new steel beam locations
- Effect of stressing sequence of PT Bars at different beam locations is investigated by nonlinear analysis (SAP2000)

Exist Bearing Pads New Bolsters

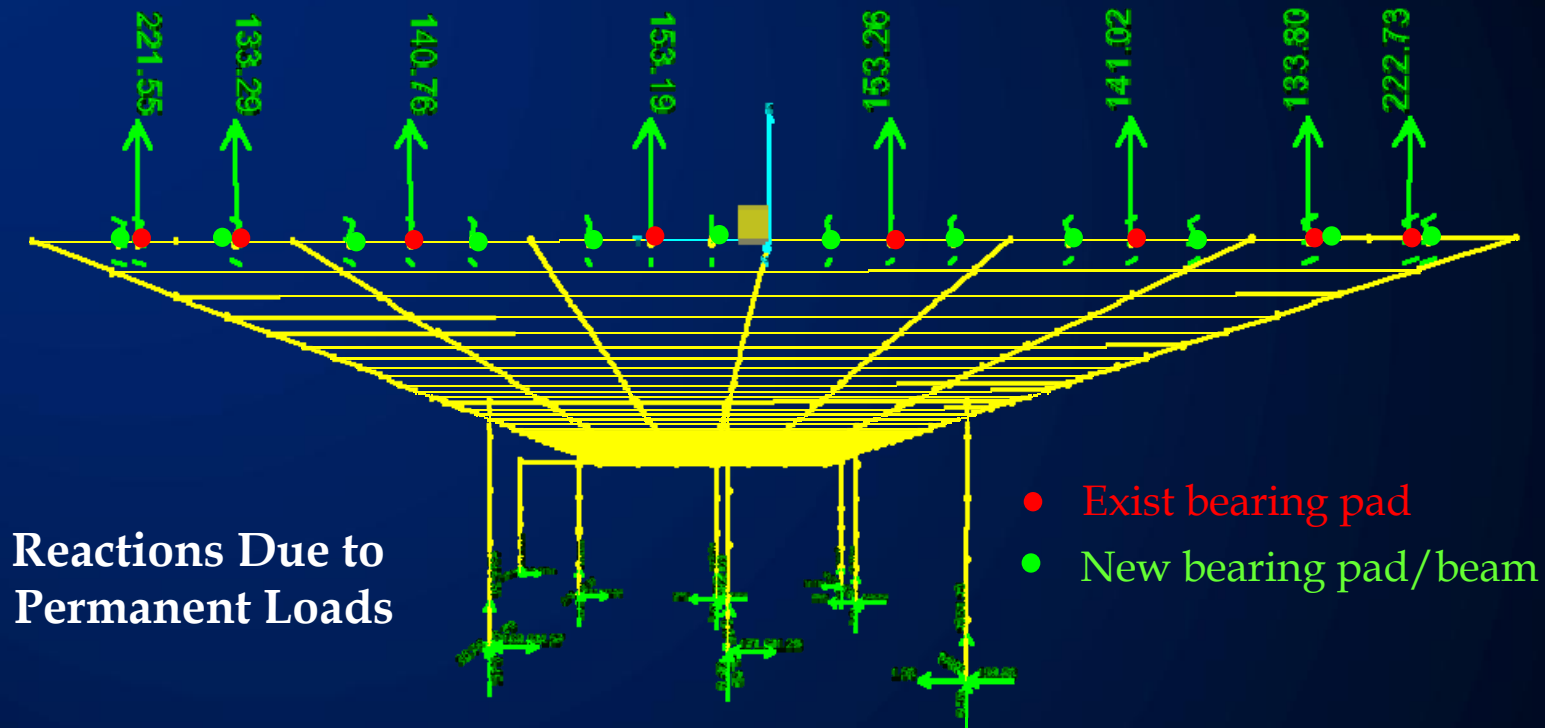


PT Bars Stressing Sequence

Grillage Model
(Frame 2 of the SB Bridge Shown)



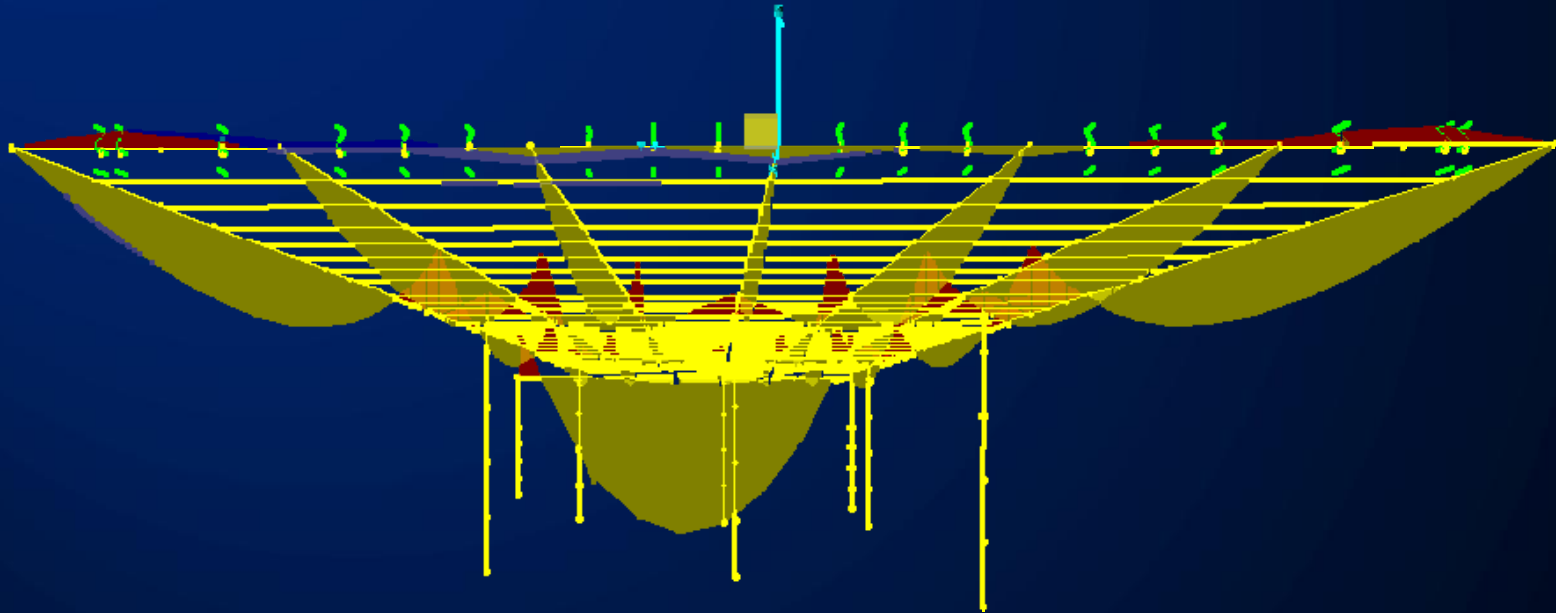
PT Bars Stressing Sequence



- Nonlinear spring (compression-only) elements used to model existing bearing pads and new steel beams/bearing pads
- Initial load case is permanent loads (reactions on existing pads only)
- Model loaded in the same sequence specified for stressing of PT bars

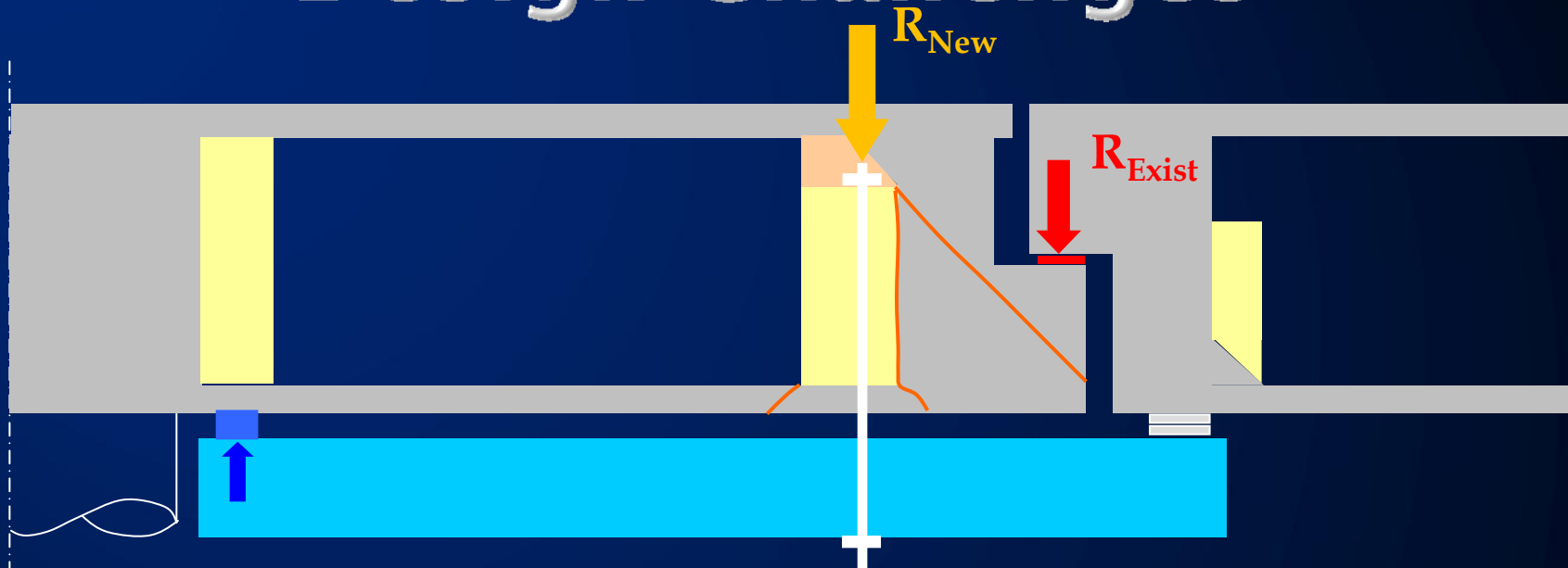
PT Bars Stressing Sequence

**Bending Moment Due to Jacking of PT Bars
at the Exterior Steel Beams (Left Side)**



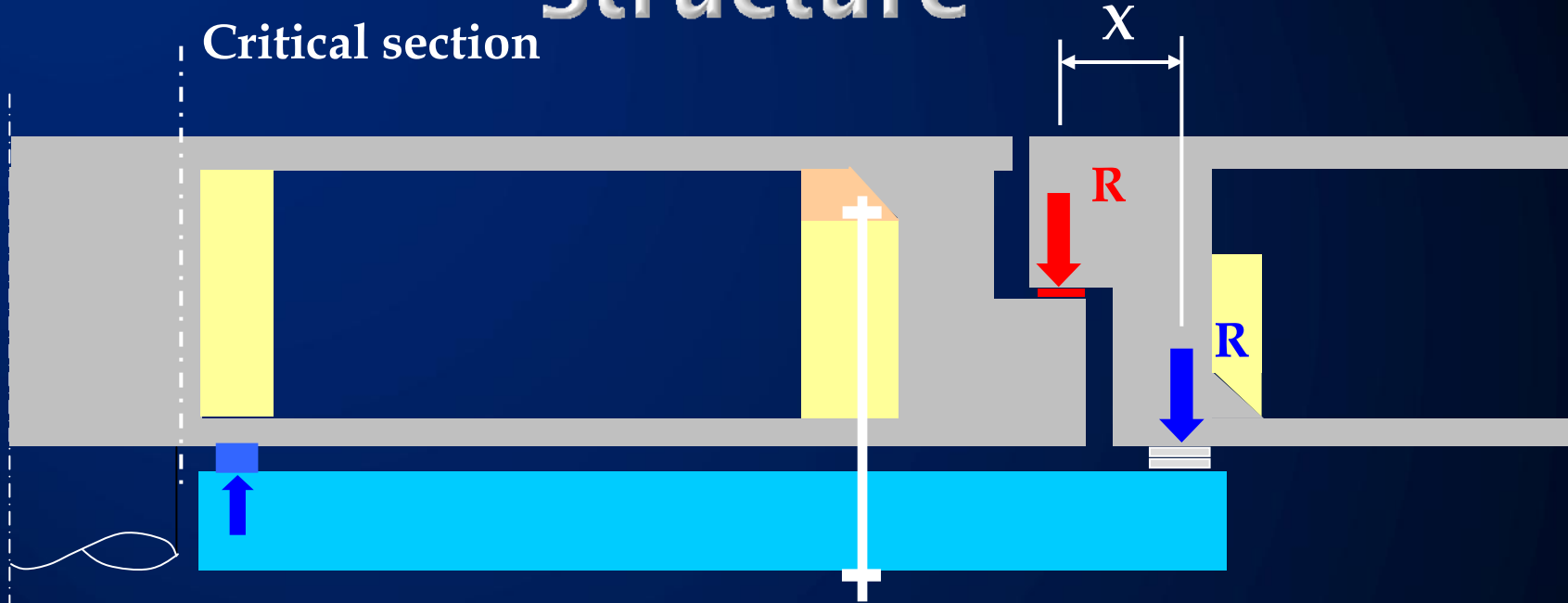
- Hinge diaphragms checked for forces due to PT bars stressing
- Bending moment is less than cracking moment and flexural capacity

Design Challenges



- New reactions on hinge diaphragm are about 50% higher than reactions in the existing condition
- Transverse analysis and check of hinge diaphragms and bolster
- Diaphragm is modelled as a beam supported on springs
- Possible failure modes of the bolster have been checked
- Special attention to design of PT Bars

Check of the Existing Structure

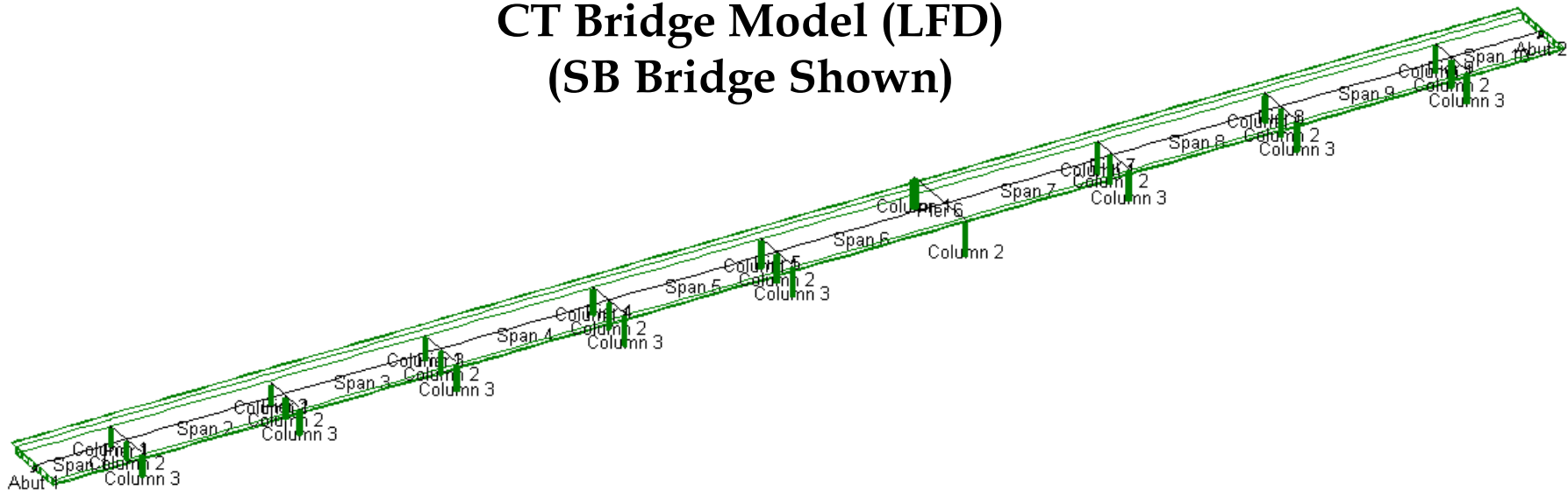


- Additional eccentricity of load on the short side of the hinge results in higher moments and tensile stresses at top of the superstructure
- Additional moment = $R \cdot X$ (X is approximately 3 ft)
- Additional moments and shears due to weight of bolsters and steel beams

Check of the Existing Structure

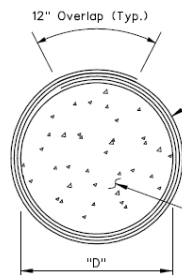
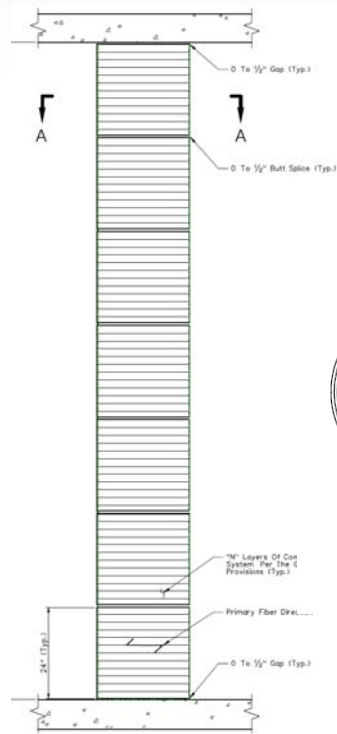
- Concrete stresses under service loads are within the acceptable limits
- Flexural and shear capacities are adequate

CT Bridge Model (LFD) (SB Bridge Shown)

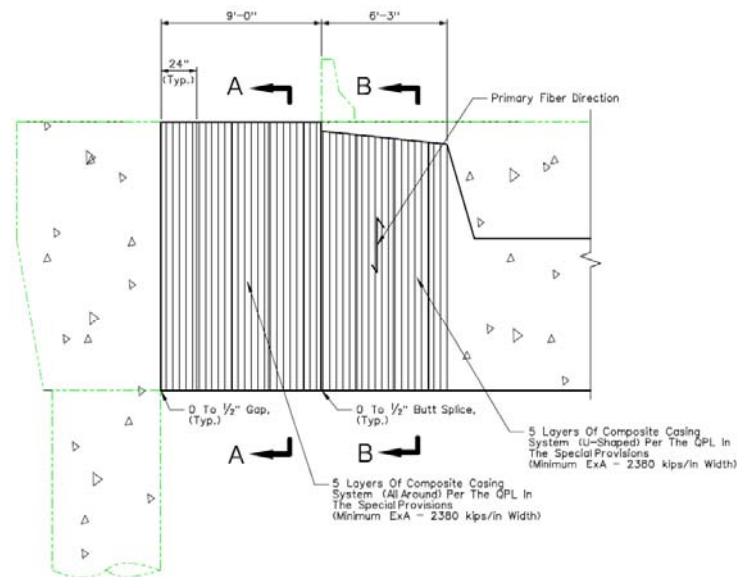


Seismic Retrofit

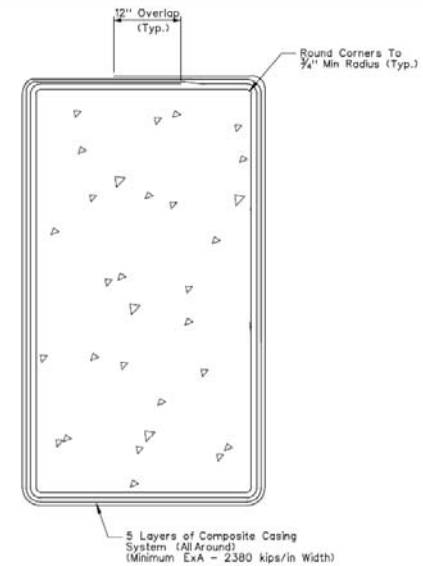
- Elastic dynamic & pushover analyses
- Displacement demand exceeds capacity for one column
- Shear demand exceeds capacity for 4 columns
- Column retrofit & outrigger bent cap retrofit by fiberwrap composite system



SECTION "A-A"



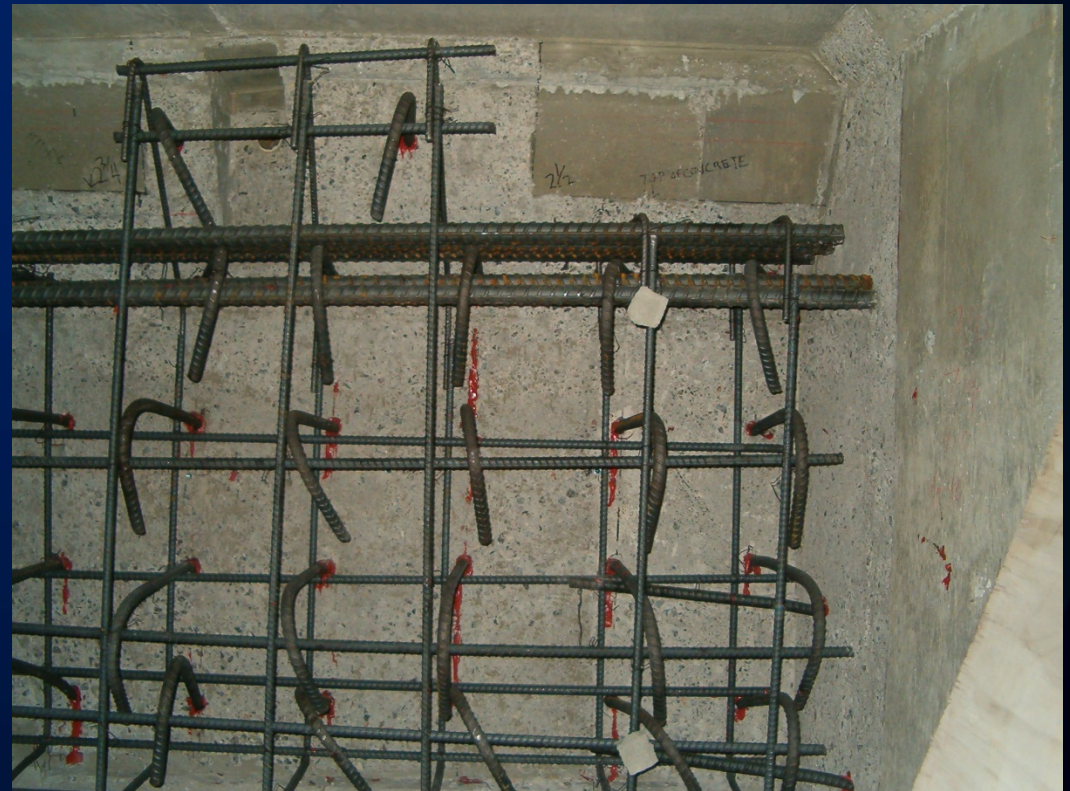
SB PIER 6 CAP ELEVATION



SECTION "A-A"

NOTE: NOT ALL LAYERS SHOWN FOR CLARITY

Construction





Summary

- ▣ Multiple Alternatives Available for Replacement of ISH (staging, aesthetics)
- ▣ External Strong Back Proved Best Alternative for This Case
- ▣ In-Depth Analysis Necessary for Force Transfer
- ▣ Scheduled Completion end of 2011

Acknowledgements

- Nevada DOT (owner, project manager)
 - Todd Stefonowicz, NDOT Bridge
- Atkins (formerly PBSJ) (prime consultant)
 - Jaime Chang and Las Vegas Team



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